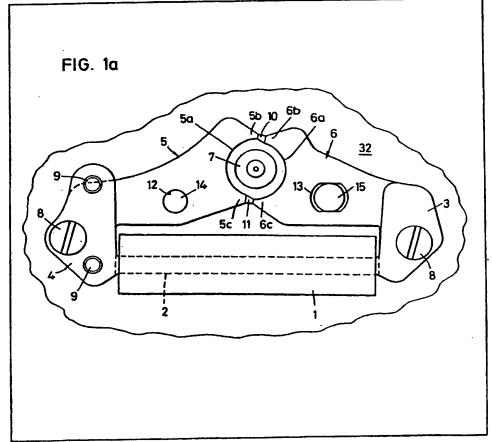
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  GB 1299952
  GB 1043277
  GB 921270
  GB 805685
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  GB 543324
- GB 212263 (58) Field of search H2A
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(54) Miniature electric motor: pole structure

(57) In a stepping motor particularly intended for electronic watches and comprising two poles 5, 6, connected to a core 2 bearing an elongated coil, the poles are joined at nose portions thereof 5b, 6b and 5c, 6c by interposed elements 10, 11 of a

material having a magnetic permeability as close as possible to 1. The one-piece stator may be formed by blanking from a composite band, then rolling together two strips of ferromagnetic metal and an interposed fillet of non-magnetic metal (e.g. brass) to join them at their edges. The stator is located on a mounting plate by pins 14, 15 and held there by screws 8.



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FIG. 1a

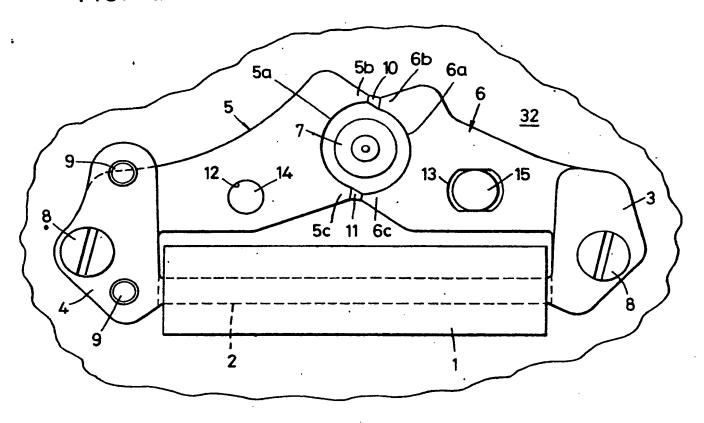


FIG. 1b

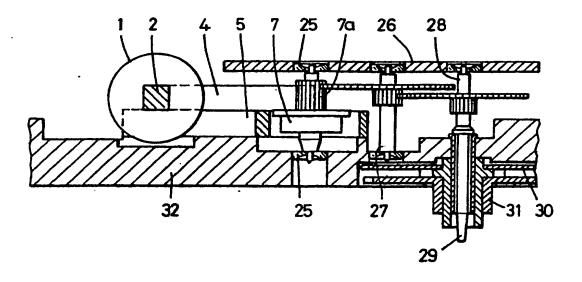
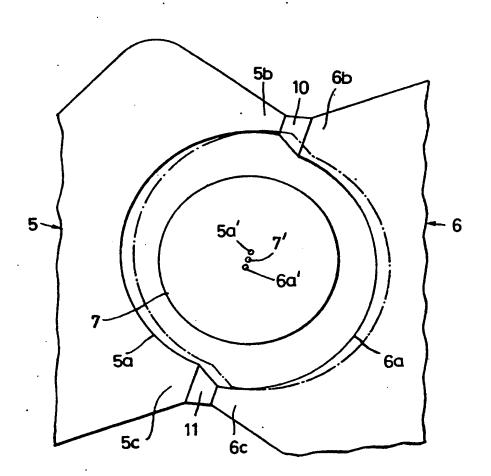
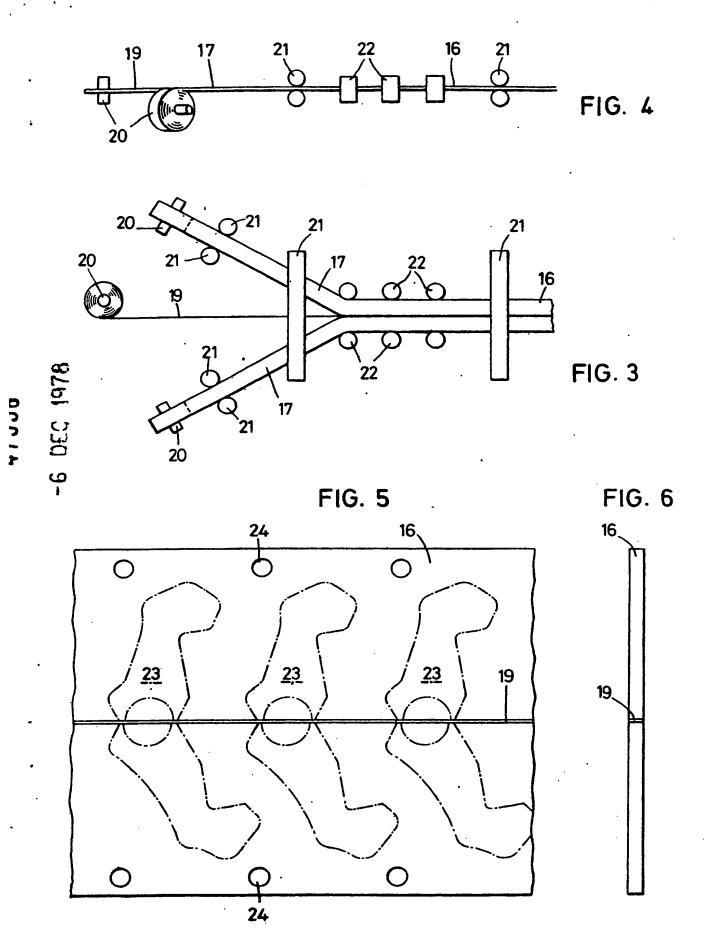


FIG. 2

-1 J





## **SPECIFICATION** Motor for electronic watch and method of manufacturing same

This invention relates to motors for electronic 5 watches, and more particularly to a motor of the type having a rotor, a magnetic coil, a core disposed in the coil, a stator having two poles, each connected to an end of the core and including two nose portions joined by a concave 10 edge embracing the rotor, and a supporting plate.

Stepping motors of this type have already been proposed (cf. U.K. Patent Specification No. 1,457,676). In general, the rotor includes a 15 cylindrical magnet having diametrical magnetization, thus exhibiting a north pole and a south pole. At each pulse, it effects a 180° rotation in a certain direction; and in order to ensure this operation, the edges of the stator poles 20 facing the rotor are blanked along an assymmetrical outline to produce an air gap having a minimum width in a specific orientation,

corresponding to the position in which the rotor stops between pulses. It is essential that the 25 orientation of the rotor upon stopping be so chosen that restarting is sure to take place in the desired direction upon the appearance of the

following pulse.

One of the advantages of motors of the 30 foregoing type is that it is possible to use rotors of very small diameter, thus having a very low inertia, which contributes towards reducing the energy to be developed at each pulse for accelerating and driving the gear-train. However, as a consequence 35 of the reduction of the size of the rotor, especially of its diameter, the stator poles must not only be blanked with extreme precision, but also positioned relative to the rotor in such a way that the shape of the gap corresponds to the desired

40 shape within an extremely narrow range of tolerance. Thus, for example, in the case of a rotor 1.6 mm in diameter, embraced by two poles having mutually offset arcuate edges, the eccentricity of each pole with respect to the axis of

45 the rotor must be 0.02 mm within a guaranteed tolerance of  $\pm 5$  microns. This requirement naturally gives rise to manufacturing and assembly problems which are difficult to solve, above all if these motors are supposed to be

 50 mass-produced, for it is necessary to be able to apply mass-production methods and to avoid adjustments and corrections during assembly as

far as possible.

Until now, efforts have been made to produce 55 the stator poles by blanking plates, each plate being provided with two positioning holes. The poles have been mounted on the plate of the watch movement, this plate including a bearing for the rotor and two pairs of positioning pins 60 engaging the poles. The poles are secured to the ends of the core bearing the coil. However, this system requires manufacturing precautions which impede mass-production.

In other types of motors, in which the stator

65 includes rigid ferromagnetic elements (cf. U.S. Patent No. 2,804,860) or a bundle of stator plates (c.f. Swiss Patent No. 259,575), designs have already been proposed in which the polepieces are joined to one another at nose portions thereof by 70 means of interposed elements of a non-magnetic metal made integral with the polepieces. These connecting elements are soldered, welded, or brazed to the polepieces. However, in these

previous designs, the stator assembly is supported 75 by rigid elements which fix the polepieces rigidly with one another. Moreover, these are designs in which the accuracy of positioning of the polepieces with respect to one another does not play any decisive part since the motors involved 80 are not stepping motors in which the shape of the poles determines the direction of rotation of the

rotor.

In the motor according to the present invention the poles are joined to one another by solid 85 elements having low magnetic permeability which make the poles integral with one another in such a way as to constitute a one-piece stator, this onepiece stator being secured on the plate.

A particularly advantageous method of 90 manufacturing the stator of this motor consists in forming the stator by a blanking operation carried out on a composite band comprising two parallel strips of a ferromagnetic material having high permeability and an interposed fillet of a material 95 having low permeability joined at its two edges to the edges of the parallel strips, thereby making them integral.

The composite band itself may be formed by simultaneous hot-rolling and welding of the two 100 strips and the interposed fillet.

A preferred embodiment of the invention will now be described in detail with reference to the accompanying drawings, in which:

Fig. 1a is a plan view of the motor,

Figure 1b is a section through the axis of the 105

Figure 2 is a partial plan view on a larger scale, showing the rotor and the parts of the poles nearest thereto,

Figures 3 and 4 are a diagrammatic plan view 110 and longitudinal elevation, respectively, on a smaller scale, illustrating the fabrication of a composite band, and

Figures 5 and 6 are a top plan view and a front 115 elevation, respectively, of the composite band from which the stators are blanked.

The motor shown in Figure 1, like conventional motors of this type, comprises an elongated coil 1 surrounding a core 2 which may, for example,

120 have a square cross-section, and the ends of which include connection clips 3 and 4 to which poles 5 and 6, embracing a rotor 7, are secured. The poles 5 and 6 are fixed to the clips 3 and 4 by screws 8. Two positioning holes 12 and 13 in the 125 poles 5 and 6 make it possible to fix the motor

assembly with respect to a plate 32 of a watch movement.

Each of the poles 5 and 6 has a concave arcuate edge 5a, 6a extending over an arc of a

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little less than 180° and, at both ends of this curved edge, two nose portions 5b, 5c, 6b, 6c. The edges 5a and 6a are offset with respect to the axis of the rotor 7, and the centers of these edges, designated as 5'a and 6'a in Figure 2, are situated one on each side of the axis of the rotor, designated as 7' in Figure 2.

As will be seen from the drawing, the poles 5 and 6 are integral with one another, for the spaces 10 between the nose portions 5b, 6b and the nose portions 5c, 6c are occupied by interposed trapezoidal elements 10 and 11 having the same thickness as the poles 5 and 6 themselves, but made of a material having low magnetic 15 permeability, i.e., practically speaking, of a material such as brass, aluminum, etc., the magnetic permeability of which is close to that of air or of a vacuum. The inverposed elements 10 and 11 situated between the homologous nose 20 portions of the poles 5 and 6 are bound by adherence to the end faces of the respective nose portions and consequently make the poles 5 and 6 integral so as to constitute a one-piece stator.

This one-piece stator is positioned on the plate 25 32 of the watch movement by the round hole 12 blanked in the pole 5 and by the elongated hole 13 blanked in the pole 6. Thus, a highly accurate positioning is obtained without exerting stress on the metal of which the one-piece stator is made. A 30 pin 14 set in the plate 32 engages the hole 12, while a cylindrical pin 15, having a diameter equal to the width of the hole 13, engages the latter. It will be noted that the centers of the pins 14 and 15 are situated on a straight line which is almost 35 perpendicular to a line passing through the centers 100 of the interposed elements 10 and 11. These positioning means make it possible to place the one-piece stator in such a way that the aperture formed by the two offset arcs 5a, 6a and the inner 40 edges of the elements 10 and 11 is as accurately centered as possible relative to the axis of the

Figure 1b shows the arrangement of the onepiece stator 5, 6 on the plate 32 of the watch 45 movement. Here the rotor 7 is seen to be situated in the central aperture of the one-piece stator. It pivots in two bearings 25 fixed to the plate 32 and to a bridge 26, respectively. The pinion 7a of the rotor 7 meshes with a first rotating part 27 which 50 likewise pivots between the bridge 26 and the plate 32 and which drives a fourth wheel-andpinion 28, the arbor 29 of which passes through the plate 32 and is intended to bear a secondshand (not shown). Other elements of the geartrain (not shown) actuate a center-wheel 30, the pipe of which bears the minute-hand, whereas a conventional minute-wheel (not shown) drives an hour-wheel 31.

By means of the pins 14 and 15 and the screws 8, the stator and the core 2 of the motor are held in place rigidly and with great precision on the plate 32, without any other assembly element.

The advantage of using a one-piece stator of the type described above during assembly is that 65 an error in centering has far less influence on

operation than if two independent poles are each positioned with slight errors relative to the rotor. Because the two poles are integral with one another, the deformation of an air gap as 70 compared with its ideal shape is compensated for by an inverse deformation of the other air gap. This is what is shown by the dot-dash line in Figure 2, which represents the position of the aperture of a one-piece stator slightly displaced as 75 compared with the ideal position. The magnetic blocking position of the rotor is practically not modified by the deformation of the air gap, the size of which increases regularly in clockwise direction despite the off-centering of the stator.

There are various ways of making the one-piece 80 stator 5, 6. Figures 3—6 illustrate a particularly advantageous method wherein the stators are formed by blanking. This method comprises a first operation consisting in fabricating a composite 85 band 16 formed of two strips 17 of ferromagnetic material and an interposed fillet 19. As may be seen in Figures 3 and 4, these three components of the band 16 are unrolled from reels 20 and are led by pairs of rollers 21 having vertical and 90 horizontal axes in such a way that the three components converge and are pressed against one another laterally by rollers 22. The operation may be carried out in a furnace with a controlled atmosphere so that the edges of the elements are welded to one another. The strips 17 are identical, may be made of iron having high permeability, for example, and will be, for example, 9 mm wide and 0.7 mm thick, whereas the interposed fillet 19 will be a ribbon of brass 0.7 mm high by 0.3 mm wide. The result is the composite band 16 shown on a larger scale in Figures 5 and 6, from which band stators 23 are blanked in the required size. The blanking operation may be carried out in a conventional swage unit, the band being 105 positioned by means of holes 24, and this operation is known to make possible guaranteed tolerances of dimensions in the micron range. The requisite precision is thus ensured by the application of methods allowing mass-production.

110 It should be noted, however, that other methods of manufacture may equally well be envisaged for obtaining the composite one-piece stators 23. Thus, for example, these stators might be blanked from strlps of homogeneous material,
115 and the areas intended to form the interposed elements 10 and 11 might then be treated in such a way as to reduce their magnetic permeability. For this purpose, operations of ion implantation, diffusion, or irradiation may be envisaged.
120 A motor provided with a one-piece stator such

120 A motor provided with a one-piece stator such as described above, with a rotor 1.6 mm in diameter, and having an air gap 0.4 mm wide in its central portion, can drive a wrist-watch gear-train by discontinuous rotation of 180° per second when energized by pulses having a duration of less than 8 ms.

## **CLAIMS**

1. A motor for electronic watches, of the type having a rotor, a magnetic coil, a core disposed in

said coil, a stator having two poles, each connected to an end of said core and including two nose portions joined by a concave edge embracing said rotor, and a supporting plate,

wherein said poles are joined to one another by solid elements having low magnetic permeability, said elements making said poles integral with one another in such a way as to constitute a one-piece stator, said one-piece stator being secured on said plate.

2. A motor in accordance with claim 1, wherein said stator is positioned by means of two fixed cylindrical pins, one of said pins being engaged in a round hole and the other in an elongated hole in

15 said stator.

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3. A motor in accordance with claim 1, wherein each of said solid elements extends between two homologous nose portions of said poles in the same plane as said poles.

4. A motor in accordance with claim 1, wherein said elements are made of a material different from that of said poles and are bonded to said nose portions by adherence.

5. A motor in accordance with said claim 1,
wherein said interposed elements are formed of
the same basic material as said poles and exhibit a
structure modified in such a way as to lower the
magnetic permeability thereof.

6. A motor in accordance with claim 1, wherein each said concave edge of said poles exhibits an arcuate outline offset with respect to said rotor, the centers of the two arcs being situated on a single

straight line passing through the axis of said rotor perpendicular to said axis.

7. A motor in accordance with claim 6, wherein said straight line passes through the centers of said interposed elements.

8. A motor in accordance with claim 3, wherein the thickness of said interposed elements is the40 same as that of said poles of said stator.

9. A method of manufacturing the motor in accordance with claim 1, wherein said stator is formed by a blanking operation carried out on a composite band comprising two thin parallel strips
45 of a ferromagnetic material having high permeability and an interposed fillet of a material having low permeability joined by the two edges thereof to the edges of said strips and making them integral.

10. A method in accordance with claim 9, wherein said composite band itself is formed by simultaneous hot-rolling and welding of said strips and said interposed fillet.

11. A motor for electronic watches,
substantially as hereinbefore described with reference to Figures 1—3 of the accompanying drawings.

12. An electronic watch having a motor as claimed in any of the preceding claims 1—8 and

60 11.

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13. A method of manufacturing a motor for electronic watches, substantially as hereinbefore described with reference to Figures 4—6 of the accompanying drawings.